

M-Smart—An Improved Multi-style Engineering Design CAD System for Clothing Thermal Functions

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Abstract

A virtual CAD system for thermal functional design is reported in this paper. An improved multi-style garment design and segmental condition specification was achieved in this system. Moreover, this system predicted the thermal status of human and clothing system while the predicted results correspond well with the experimental results. Both 3D static and dynamic visualization were presented to the users to get a feedback for the design case.

Keywords: Thermal Functional Engineering Database; Multi-style Garment Design; Cad System; Segmental Specify

1 Introduction

With the application of CAD technologies in thermal functional design area, designers can perform virtual garment design on a computer instead of doing experimental tests in laboratories. This does not only reduce the development period but also saves significant costs involved in conducting testing experiments. Published papers and models can be found extensively, describing the heat and moisture transfer process between human and multi-layer fabrics which provides the theoretical foundations and possibilities for CAD functional design.

In previous researches, a CAD system named P-smart for multi-layer clothing thermal engineering design had been developed to predict the thermal status of both human and clothing during a series of activities [1]. With P-smart system, designers can design the clothing in a virtual environment with the assigned activities and predict the thermal status of both human body and clothing. Compared to the traditional clothing testing methods, P-smart allowed designers to perform the clothing design on a computer which reduces the design period. Moreover, P-smart

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model for human body and a mathematical model describing the heat and moisture transfer process through multi-layer garments.

2.1 Human Regulation Model

In the passive system of Stolwijk's model (Stolwijk and Hardy, 1997), the body is composed of head, trunk, arms, hands, legs and feet segments which are subdivided into four concentric layers representing the core, muscle, fat and skin layers. An additional node called center point denotes the central blood pool which executes the communication among the six segments via convection heat exchange occurring within the blood flow of each node.

Passive system:

$$\begin{cases} C_n \frac{dT_n}{dt} = Q_i - B_i - D_i - E_i & n = 1, 2, \dots, 24 \\ C_b \frac{dT_b}{dt} = \sum_{n=1}^{24} B_n \end{cases} \quad (1)$$

$$\begin{cases} \text{Core layer: } Q(N) = QB(N) \\ \text{Muscle layer: } Q(N+1) = QB(N+1) + WORKM(I) * (WORK) + \\ \quad CHILM(I) * CHILL \\ \text{Fat layer: } Q(N+2) = QB(N+2) \\ \text{Skin layer: } Q(N+3) = QB(N+3) \end{cases} \quad (2)$$

$$\begin{cases} \text{Core layer: } BF(N) = BFB(N) \\ \text{Muscle layer: } BF(N+1) = BFB(N+1) + Q(N+1) - BFB(N-1) \\ \text{Fat layer: } BF(N+2) = BFB(N+2) \\ \text{Skin layer: } BF(N+3) = \frac{BFB(N+3) + SKIVN(I) * DILAT}{(1 + SKINC(I) * STRIC) * 2^{(ERROR(N+3)/10)}} \end{cases} \quad (3)$$

In the controlling system of Stolwijk's model (Stolwijk and Hardy, 1997), four types of thermal reactions of the body are considered which include shivering, sweating, vasoconstriction and vasodilatation process. Based on the computational results, the effects of the metabolic rate, blood flow, sweating and shivering can be obtained. The controlling system can be described as follows.

Controlling system:

$$\begin{cases} \text{SWEAT} = \text{CSW} * \text{ERROR}(I) + \text{SSW} * (\text{WARMS} - \text{COLDS}) + \\ \quad \text{PSW} * \text{WARM}(I) * \text{WARMS} \\ \text{DILAT} = \text{CDIL} * \text{ERROR}(I) + \text{SDIL} * (\text{WARMS} - \text{COLDS}) + \\ \quad \text{PDIL} * \text{WARM}(I) * \text{WARMS} \\ \text{CHILL} = -\text{CCHIL} * \text{ERROR}(I) + \text{SCHIL} * (\text{COLDS} - \text{WARMS}) + \\ \quad \text{PCHIL} * \text{COLD}(I) * \text{COLDS} \\ \text{STRIC} = -\text{CCON} * \text{ERROR}(I) + \text{SCON} * (\text{COLDS} - \text{WARMS}) + \\ \quad \text{PCON} * \text{COLD}(I) * \text{COLDS} \end{cases} \quad (4)$$

$$\left\{ \begin{array}{l} \text{ERROR}(N) = T(N) - \text{TEST}(N) + \text{RATE}(N) * F(N) \\ \text{WARM}(N) = \text{ERROR}(N) \quad \text{ERROR}(N) > 0 \\ \text{COLD}(N) = \text{ERROR}(N) \quad \text{ERROR}(N) < 0 \\ \text{WARMS} = \text{SKINR}(1) * \text{WARM}(4) + \text{SKINR}(2) * \text{WARM}(8) + \\ \quad \text{SKINR}(3) * \text{WARM}(12) + \text{SKINR}(4) * \text{WARM}(16) + \\ \quad \text{SKINR}(5) * \text{WARM}(20) + \text{SKINR}(6) * \text{WARM}(24) \\ \text{COLDS} = -\text{WARMS} \end{array} \right. \quad (5)$$

2.2 Mathematical Models for Heat and Moisture Transfer Process in Clothing

When a water vapor concentration gradient exists across the multi-layer textile, the moisture flux can be re-distributed due to the diffusion process through the void space in the textile. The governing (Burley's model) equation describing the vapor transfer process is given based on the diffusion law and Li and Luo's two-stage absorption model.

$$\frac{\partial(\varepsilon_a C_a)}{\partial t} = \frac{D_a \varepsilon_a}{\tau_a} \cdot \frac{\partial^2 C_a}{\partial x^2} \frac{\varepsilon_a}{\varepsilon} \varepsilon_f \cdot \frac{\partial C_f}{\partial t} + \tau_{lg} \quad (6)$$

The liquid water diffusion through textile can be attributed to a capillary process through fabrics. The mathematical descriptions for the process of liquid transfer, moisture sorption/desorption and condensation/evaporation can be expressed as follows.

$$\frac{\partial(\rho_1 \varepsilon_1)}{\partial t} = \frac{\partial}{\partial x} \left(D_1(\varepsilon_1) \frac{\partial(\rho_1 \varepsilon_1)}{\partial x} \right) - \frac{\varepsilon_1}{\varepsilon} \varepsilon_f \cdot \frac{\partial C_f}{\partial t} - \tau_{lg} \quad (7)$$

The heat transfer process happens along with the process of conduction, convection and radiation while the conduction and radiation of heat plays a predominant role in energy transfer. The governing equation for heat transfer process can be written as follows.

$$c_v \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left(K_{\text{mix}}(x) \frac{\partial T}{\partial x} \right) + \frac{\partial F_R}{\partial x} - \frac{\partial R_L}{\partial x} + c_r \cdot \frac{\partial C_f}{\partial t} \left(\frac{\varepsilon_a}{\varepsilon} \cdot \lambda_v + \frac{\varepsilon_1}{\varepsilon} \cdot \lambda_1 \right) - \lambda_{lg} \cdot \tau_{lg} \quad (8)$$

3 M-smart System Introduction

To design M-smart system, the architecture and computation flow are the key points. Based on a thermal functional database, which includes human model databases and functional garment database, the designed class structure illustration figure shows the relationship between different kinds of objects.

3.1 M-smart System Architecture

The CAD system is built on thermal engineering database which includes two parts: human model and multi-style garments. The architecture of the CAD system is demonstrated in Fig. 2. It can be found that the pre-simulation process is related to the database of the human and garment definition steps. Moreover, the human model and garments in the visualization process are also downloaded from the thermal engineering database.

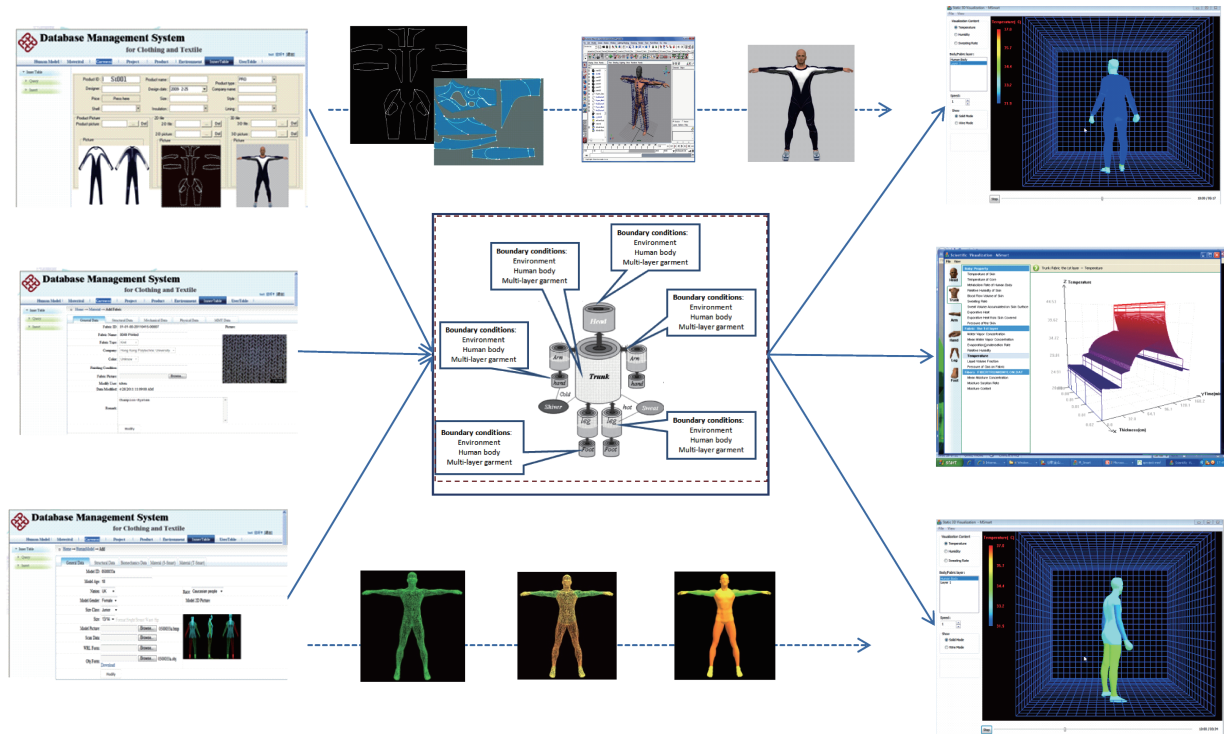


Fig. 2: Architecture of M-smart system

3.2 Numerical Simulation Flow Chart

With the pre-simulation process, the parameters for the calculation process are prepared. The calculation for the heat and moisture transfer process in clothing is based on a finite volume method. The human regulation calculation can be translated into linear equations computation. The thermal status of the human skin surface can be the boundary condition for the dynamic calculation of clothing. The simulation flow chart can be understood from Fig. 3.

3.3 Class Design

This CAD system is programmed in C++ language and classes design is also adopted in this system. The class relation is illustrated in Fig. 4.

4 Design Case

In order to illustrate the thermal comfort predictability of this CAD system, a case of summer running protocol is introduced and a comparison of simulation results and experimental results with body core temperature and skin temperature is evaluated.

4.1 Case Design Specification

In order to investigate an athlete's running process, a series of activities is extracted from the experiment process. With the environment in the chamber maintained as 30C and 50% RH, the

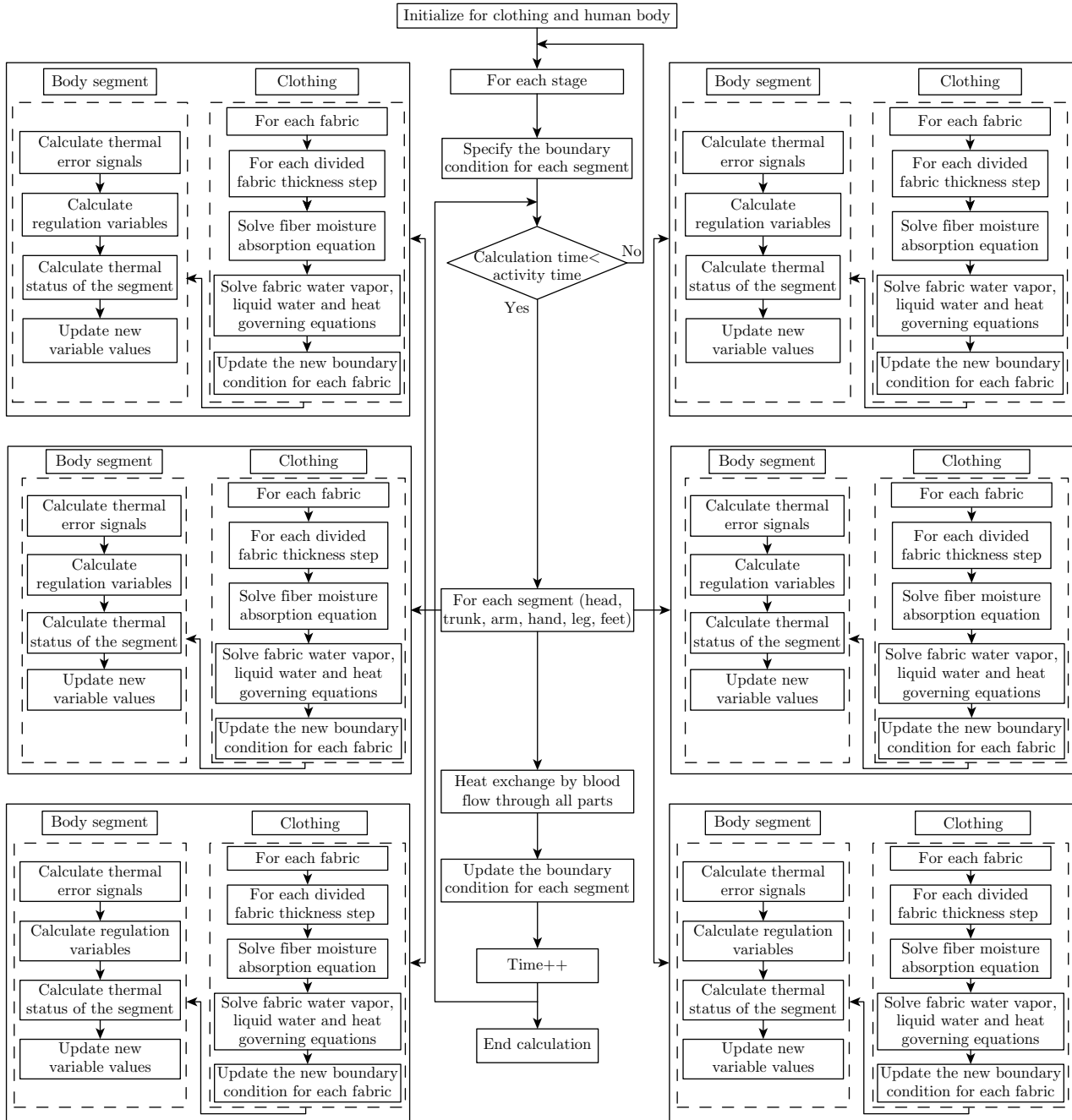


Fig. 3: Simulation flow chart of M-smart system.

velocity during the resting process is 0.2 m/s, whilst during the whole running process the velocity is 3.5 m/s (positive going to the athlete). The experiment can be described by five continuous motor processes which are: seated resting for 30 min at a metabolic rate of 58 W/m², warm up running for 10 min at 400 W/m², 70% VO₂ max running for 45mins at a metabolic rate of 550 W/m², 1500 performance running for 5min at a metabolic rate of 650 W/m², then recovery for 30 min at a metabolic rate of 60 W/m². The wind velocity during the first and last stages is 0.2 m/s while the wind speed during the other three running processes is 3.0 m/s. Fig. 5 illustrates the running protocol.

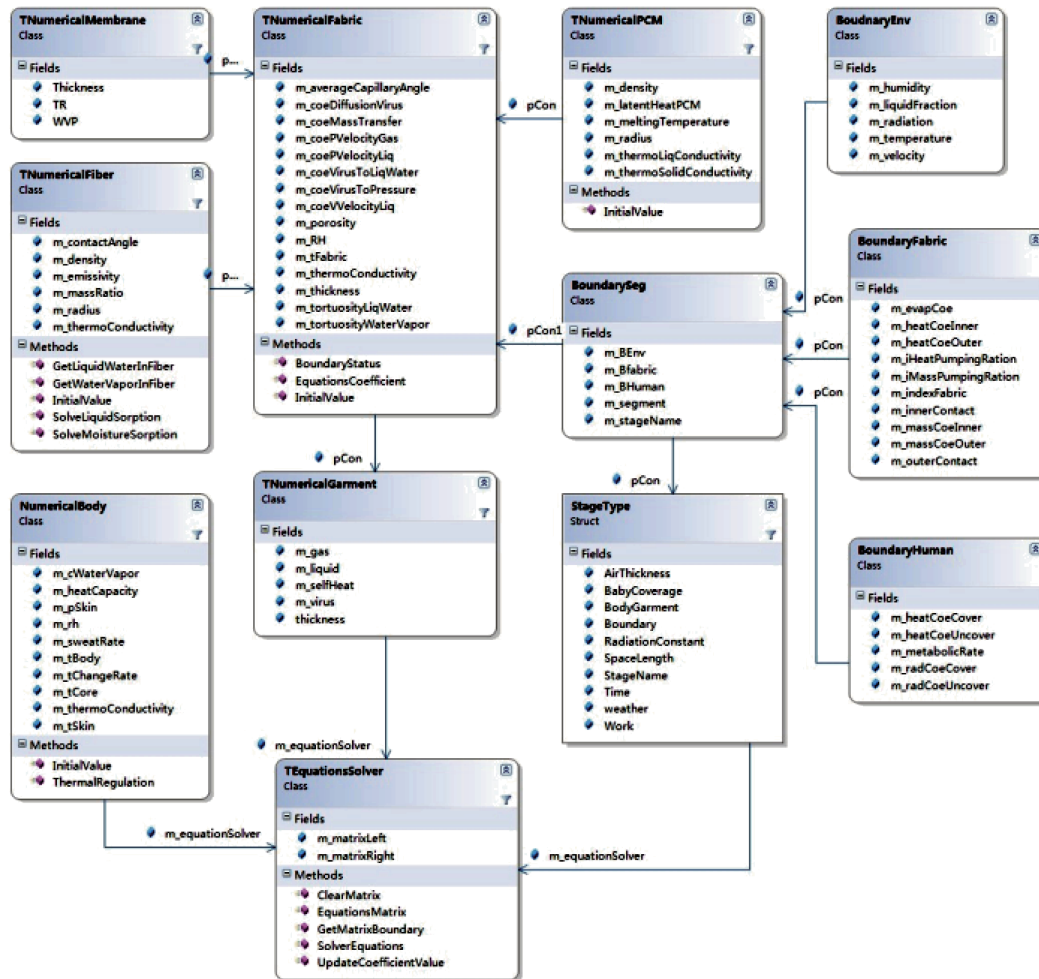


Fig. 4: The class relation diagram of M-smart.

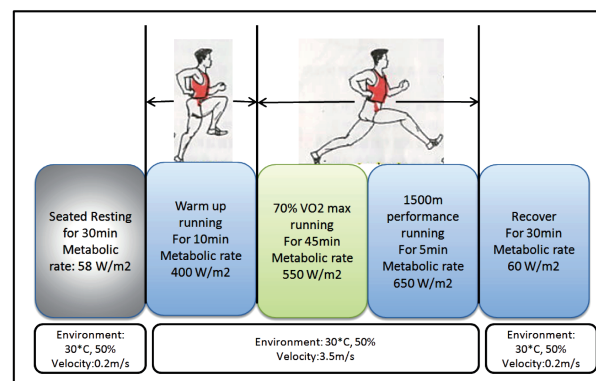


Fig. 5: Experimental protocol.

4.2 Multi-style Simulation Case Design

Based on the experimental testing, the simulation case design process can be divided into six steps.

Step 1: Define the activity stages including the activity clarification, metabolic rate and dura-

tion. The interface can be found in Fig. 7.

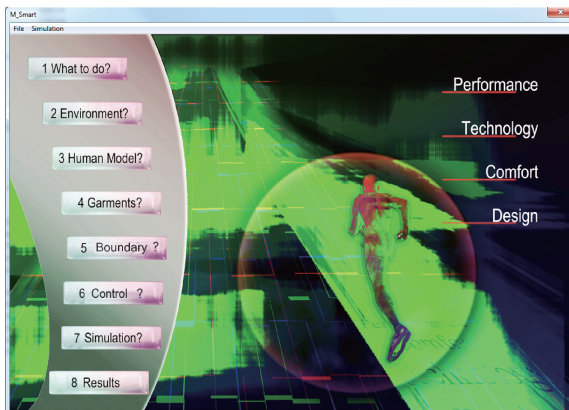


Fig. 6: The main interface of M-smart system

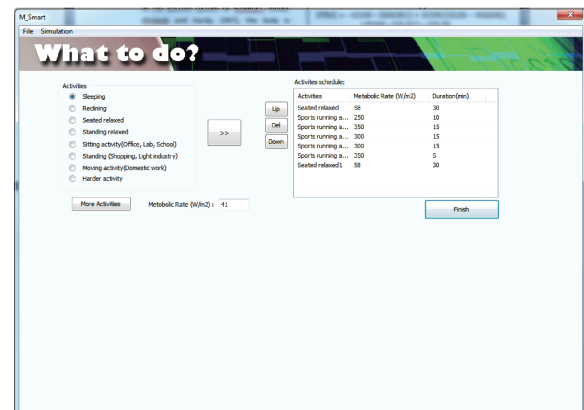


Fig. 7: Step 1: What to do?

Step 2: Define the environmental condition for each stage including temperature, relative humidity, wind velocity and air pressure. These values will be default values for the boundary condition specification.

Step 3: Choose the human basic condition then search from the database to obtain a close human model and identify the physiological data according to the human size.

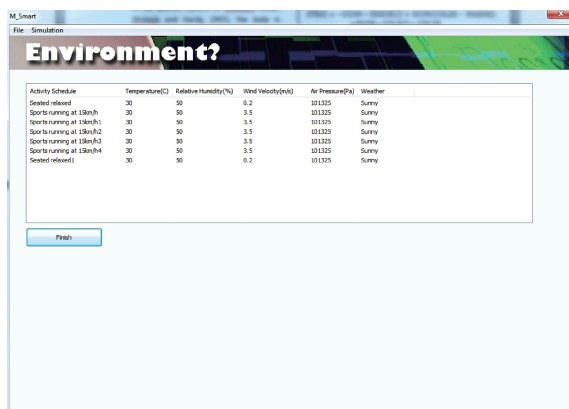


Fig. 8: Step 2: Environment?

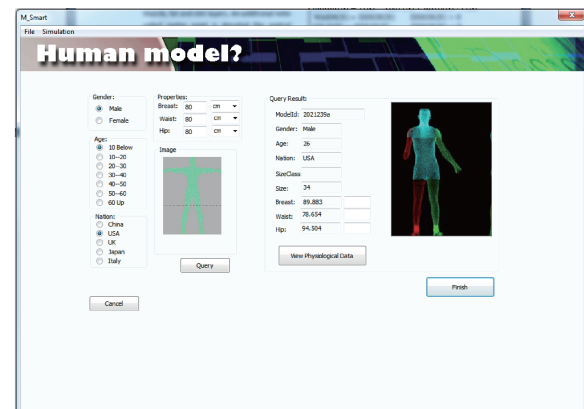


Fig. 9: Step 3: Human model selection panel

Step 4: Define the multi-style garment. Choose the garment from the garment list. All the garments are downloaded from the garment database while the size of the garment is the same as the human model chosen in step 3.

Then, define the garment one by one. For one garment, this CAD system separates into six parts. Each part can have at most three fabric layers and a cover ratio.

Specify the fabric parameters to a layer on one segment. The fabric information includes the fiber ingredient, the fabric thickness, radius, the contact angle and MMT characters.

Step 5: Segmental boundary condition specification. For each stage and each segment, set the specified value according to the intensity of the activity.

After completion of the above mentioned steps, the simulation process can start.

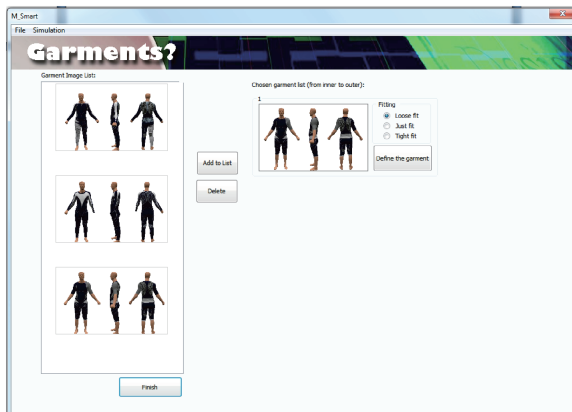


Fig. 10: Step 4: Multi-style garment definition panel

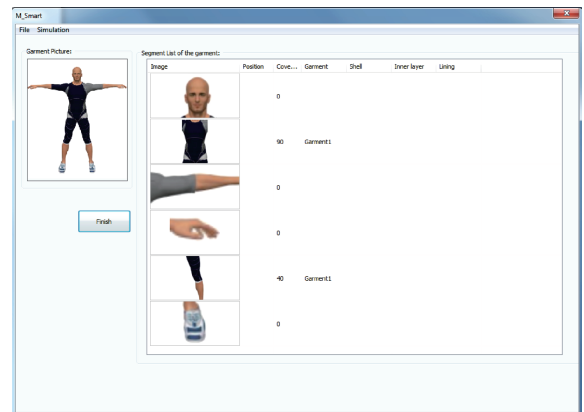


Fig. 11: One garment definition panel

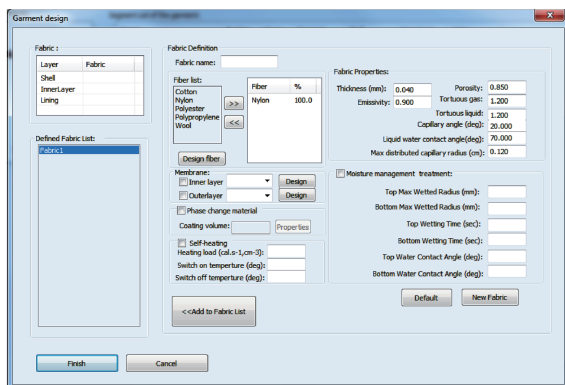


Fig. 12: Fabric definition panel

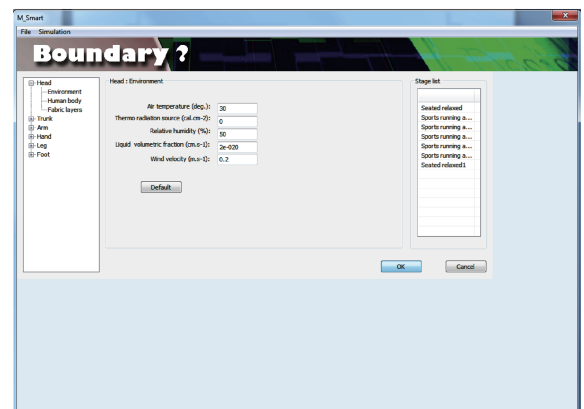


Fig. 13: Step 5: Boundary condition specification

4.3 Validation of the Simulation Case

In the previous steps, the running protocol, environment, human model, multi-style garments and boundary conditions are specified. The thermal status which demonstrates the thermal status changing tendency of human body is presented. The key index of human thermal status is the core temperature of human body. From Fig. 14, it can be found that the predicted data agrees well with the experimental data at each stage.

From Fig. 15, the changing tendency of the mean skin temperature is almost the same as the value changes in the 5% error bar range.

4.4 3D Visualization

A three dimensional visualization is provided in M-smart system. Fig. 16 shows a 3D human model which is selected from the human model selection module downloaded from the human model database. The cross section shows the core and skin temperature of the selected segment.

The 3D human model with the selected garment can also be shown in this panel. Choose the garment and watch the thermal status changes during this process (Fig. 17).

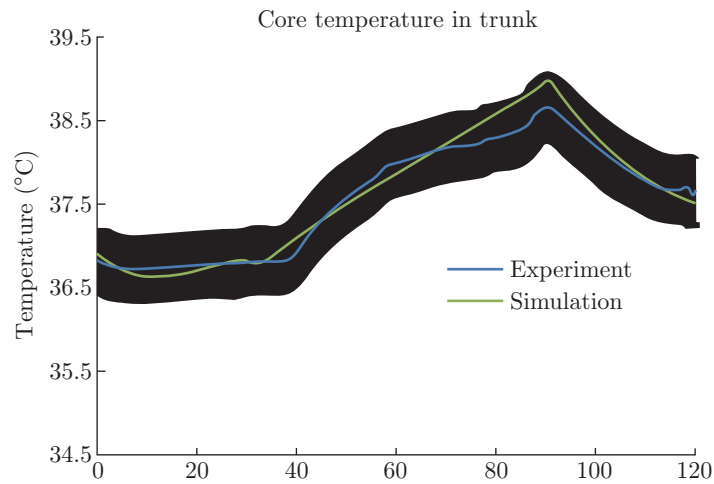


Fig. 14: Core temperature comparison

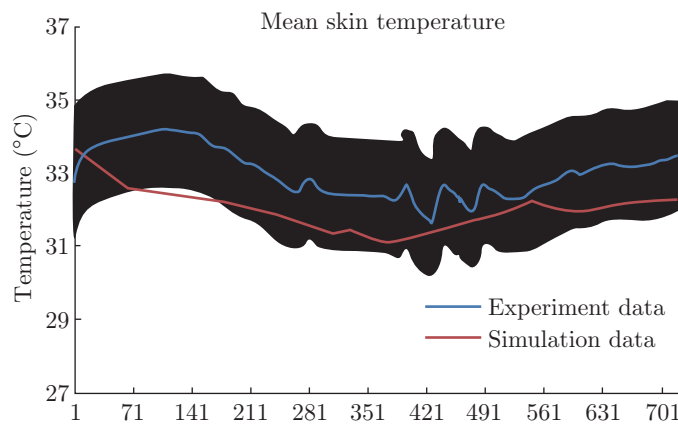


Fig. 15: Mean skin temperature comparison

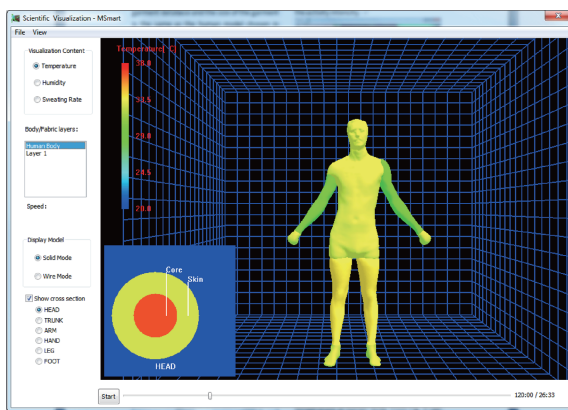


Fig. 16: Static 3D human model visualization presentation

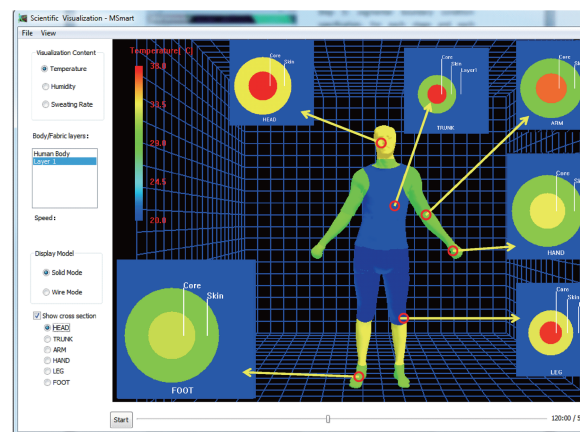


Fig. 17: Static 3D human model with garment visualization presentation

Fig. 18 shows a 3 dimensional visualization. The human model is a standard human model from 3D software. As the 3D model can do a series of activities which is called dynamic, choose the human model to observe the thermal status changes during the motor process.

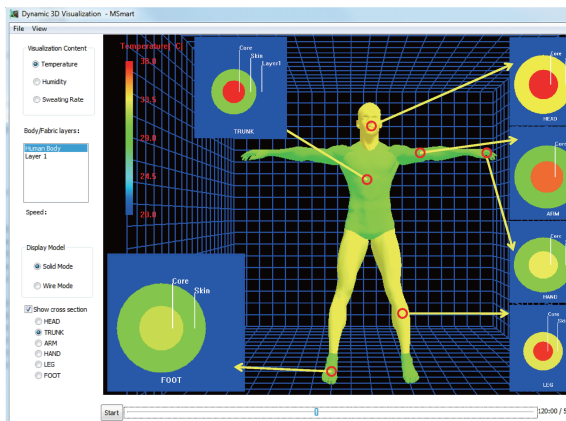


Fig. 18: Dynamic 3D human model visualization

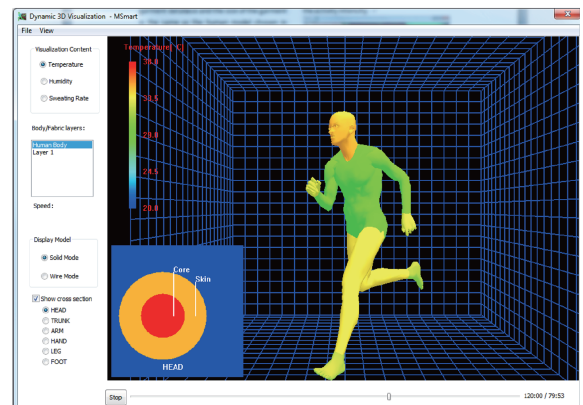


Fig. 19: Dynamic 3D human model visualization at running status

5 Conclusion

The simulation results show different responses to different scenarios. The comparison between simulation results and experimental results indicates that the improved CAD system can predict the heat and moisture process in human-clothing system.

This improved system includes four parts: thermal functional engineering database, friendly user interface, simulation calculation and visualization. The relationship among these four parts can be described as: the thermal functional database is the basic platform for the whole system. The pre-simulation process is to collect all the calculation parameters and store them into a pre-simulation file. Then, pass the file to calculation process to obtain the simulation results, which will be presented in the visualization part.

The CAD system can realize a true multi-style garment design. Moreover, segmental garment design and calculation is adopted in this CAD system.

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